The LPG gas-sensing performance of CeO$_2$-CuO nanocomposite film synthesized by microwave assisted sol-gel method

Kabure A. A., Mane S. R., and Shirke B. S.

1*Material Science Laboratory, Department of Chemistry, Y. C. Warana Mahavidyalaya, Warananagar, India
2Department of Chemistry, K. R. P. Kanya Mahavidyalaya, Islampur, India

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INTRODUCTION

This work is the beginning stage in our investigation of gas sensor properties regarding LPG of different CeO$_2$-CuO structures obtained by microwave assisted sol-gel method. There are different methods for the synthesis of ceria nanocomposite such as solvothermal synthesis, thermal decomposition, microwave assisted sol-gel, solution precipitation, hydrothermal crystallization, mechanochemical, sol–gel and thermal hydrolysis [1, 2, 3]. But, microwave assisted sol-gel method has advantages like consequent dramatic increase in reaction rate, high reaction yields, reaction selectivity, and ease of handling. Here, heating arises from dipole rotation or ion migration, which then produce fast homogeneous nucleation and easy gel dissolution [1]. Microwave synthesis of metal oxide nanoparticles is simple, economic, selective process, consumes less energy and fast production speed with better quality [4, 5]. Ceria and ceria-based oxide materials are the functional rare-earth oxides for their wide applications in gas sensing, environmental chemistry, catalysts, solid oxide fuel cells (SOFC), oxygen membranes, metal-oxide semiconductor devices. The morphology and nanostructure are two essential factors in the functional performance of ceria and ceria-based oxide materials [6]. Nanocrystalline and porous CeO$_2$ offer high affinity for the development of lots of oxygen vacancies due to the practical redox potential of Ce and the ability to maintain the electro neutrality of the Ce and O species. The consolidation of a foreign metal, for example, lanthanide or transition metals onto the CeO$_2$ lattice can change its chemical and electronic properties and is therefore expected to advance the redox properties of CeO$_2$ in the final metal/oxide composition, which leads to higher oxygen mobility [7]. Nanocrystalline Cu-based materials have been indicated remarkable execution in gas-phase

Key Words:
CeO$_2$, Nanocomposites, HRTEM, SEM, X-Ray Diffraction, LPG, Gas Sensor

ABSTRACT

High demand of semiconductor gas sensors works at low operating temperature has led to the fabrication of gas sensor based on CeO$_2$ nanoparticles. The aim of the work was to obtain CeO$_2$-CuO nanocomposites with heightened surface area by a simple microwave assisted sol-gel method and to study gas sensing properties towards propane-butane mixture (LPG). The morphological and structural properties of the sensing film were characterized by X-Ray Diffraction (XRD), Transmission Electron Microscope (TEM), Scanning Electron Microscope (SEM) and UV-Visible spectroscopy technique. A CeO$_2$-CuO nanocomposite has a well-defined cubic structure with a crystallite size of ~10 nm. Spherical shapes of the as prepared nanocomposite were observed under HRTEM. The SEM image of CeO$_2$-CuO nanocomposite displays spongy-like features with large voids and small spherical agglomerates of CuO, which is useful in gas sensing application. It is found that the CeO$_2$-CuO system includes CeO$_2$ surface sites with oxygen vacancies for oxygen sorption. The XRD patterns of composite samples revealed distinct peaks of CeO$_2$ and CuO, which clearly indicates formation of CeO$_2$-CuO nanocomposites. An optical analysis shows the lowering of band gap energy from 3.19 eV (E$_g$-CeO$_2$), 1.7 eV (E$_g$-CuO) to 1.3 eV (E$_g$-CeO$_2$-CuO). The gas sensing behavior of the pure and composite sensor was systematically investigated for the target gas LPG. Under optimum operating temperature of 275°C and 24 ppm LPG, the CeO$_2$-CuO sensor showed maximum response of 57.09%. The response and recovery time of CeO$_2$-CuO sensor for LPG was found to be ~25 s and ~50 s, respectively. The CeO$_2$-CuO sensor showed better response than pure CeO$_2$ and CuO sensor, which is attributed to n-p heterojunction at the intergrain boundaries.

*Corresponding author: Dr Shirke B. S
Material Science Laboratory, Department of Chemistry, Y. C. Warana Mahavidyalaya, Warananagar, India

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reactions. Hence, CuO is chosen for sensing application which has unique properties like high specific surface area, chemical stability, electrochemical activity, high electron communication features [8]. The fundamental concern right now is focused particularly on the surface conductive metal oxide gas sensors. The main feature of conductometric semiconducting metal oxide gas sensors is reversible interaction of the gas with the surface of the material [9]. Specifically, the composite of copper oxides (CuO) and cerium oxide (CeO₂) is of great interest because of their catalytic and redox activities [10, 11]. A few examinations on Ce-Cu-O redox frameworks have recommended that change in the oxidation state of both Ce and Cu in ceria-copper framework; can promote the rate of reaction at the metal oxide interface [12-15]. Such a redox mechanism is succeeded by the formation of a Cuᴵᴵ⁺ species (Cu²⁺↔Cu¹⁺) in CuO, which is related with the reduction of adjacent CeO₂ (Ce⁴⁺↔Ce³⁺) [16]. The activity of CuO/CeO₂ catalysts is related to the highly dispersed CuO species, its strong interaction with CeO₂, and mutual effect between Cu¹⁺/²⁺ and Ce³⁺/⁴⁺ redox couples [17]. The multi valence state of cerium leads to remarkable properties of the material such as oxygen storage and releasing capacity [18, 19]. The large surface area to volume ratio existing in a nanoparticle allows CeO₂ to react differently resulting in unique properties [8, 20]. It is notable that, the dispersion and valence state of copper species, solid solution, and oxygen vacancies associated with the synergistic interaction and catalytic performance rely on the preparation methods [10]. For example, Wang et al. [21] reported that, the solvent-free method facilitated the formation of synergistic interaction between copper species and ceria to result in smaller crystallite size and the formation of more Cu⁻ species together with a high ratio of Ce³⁺. Shang et al. [22] showed that, the impregnation method offered highly dispersed CuO and stronger synergistic interaction between CuO and CeO₂ to promote the reduction of CuO to Cu⁻ species at the Ce–Cu interface, resulting in the highest catalytic activity. Highly sensitive gas detecting devices has expanding demand in several applications. An effective strategy to improve sensor execution is to embrace the nanostructured sensing materials that have a high surface area to volume ratio and consequently a strong interaction arises between the surrounding gas and the material [23]. Presently, liquefied petroleum gas (LPG) is an energizing option in contrast to regular energy sources, because of its abundance and low cost [24]. The LPG is a combustible blend of hydrocarbon gases used as fuel in many applications like industries, homes, vehicles, hostels, automobiles on account of its attractive properties which incorporate high calorific value, less smoke, virtual lack of sulphur; which brings about clean burning and less harm to the environment [25]. Among various gases, the probability to control propane-butane mixture (LPG) content in air is of high importance due to its high explosiveness [26]. Sensitivity has been drawing in more consideration, as one of the significant parameters of gas sensors and much exertion has been made to improve the sensitivity of gas sensors. The authors have proved that the increase in the temperature up to a certain value leads to heightening in the sensitivity. On the other hand, the further temperature growth results in the decrease in the sensor sensitivity. Thus, there is an optimum temperature value corresponding to the maximum sensitivity of the sample. The objective of this study is to determine the ideal method and technological parameters corresponding to formation of material with the highest sensor response.

Experimental

Materials and chemicals

All the chemicals used for the preparation were of analytical grade. It includes cerium nitrate [Ce(NO₃)₃·6H₂O] (99%), copper chloride [CuCl₂·2H₂O] (99%), propylene glycol [C₃H₆O₂] and ammonia. All the solutions were prepared in distilled water.

Synthesis of nanocomposite material

The CeO₂ powder was prepared by the microwave assisted sol-gel method. All the chemical reagents used without further purification. Cerium nitrate and propylene glycol were used as starting precursors. Mixture of 0.1M aqueous solution of cerium nitrate and propylene glycol was prepared with ratio of concentration 1:1. The CeO₂ metal oxide powder preparation was achieved with dropwise addition of aqueous ammonia [NH₃·H₂O] to the above mixture with constant stirring. The addition of aqueous ammonia was continued until the solution reached pH = 10. After complete gel formation, that gel hydroxide was washed with distilled water. Then pure hydroxide in a glass beaker was placed in a microwave oven (in put power 600W) for about 30 minutes with on-off cycle. The obtained oxide sample was crushed to prepare fine powder. In the same way, CuO powder was prepared by using copper chloride. For the synthesis of CeO₂–CuO composite, same procedure was followed, by mixing solution of copper chloride and cerium nitrate.

Fabrication of the sensing film

The paste of CeO₂–CuO nanocomposite was prepared by mixing the resulting CeO₂–CuO nanopowder with a temporary binder as a mixture of organic solvent. The ratio of inorganic to organic part was kept as 80:20 in formulating the paste. The paste was then used to prepare thin films on substrate in desired pattern of size (4 mm × 9 mm) by screen-printing technique. These films were dried and cured at 80°C, followed by firing at 200°C for 30 min in air ambient atmosphere. Silver contacts were made by vacuum evaporation for gas sensing measurements. The sensing performance of the sensors was examined using a static gas sensing system. There are electrical feeds on the base plate, a heater was fixed on the base plate. The sample under test was mounted above the heater. A Cr–Al thermocouple was mounted on the heater to measure the operating temperature of the sensor. The required gas concentration inside the static system was achieved by injecting a known volume of test gas by a gas-injecting syringe. A constant 10 V d.c. voltage was applied to the thin film of CeO₂–CuO and current was measured by a
multimeter. The air was allowed to pass into the glass dome after every LPG gas exposure cycle.

**Characterization of nanocomposite material**

The X-ray diffraction of the powder samples were measured on ‘Rigaku Miniflex 600’ diffractometer with Cu-Kα radiation (λ=1.5405Å) operating at 45 kV and 100 mA over a range of 2θ from 10° to 80°, at a scanning rate of 5°/min. HRTEM study of the powder sample was carried out by using model number JEE-2100, (JEOL) 200KV (SAIF-NEHU, Shillong). The surface morphology of the films was analyzed using a SEM [scanning electron microscope model JEOL 6300 (LA) Germany]. The UV-Visible (UV-Vis) absorption spectra were recorded in a ‘Jasco (model V-770) UV-Vis-NIR Spectrophotometer’ in the wavelength range 200 to 800 nm.

**RESULTS AND DISCUSSION**

**X-Ray Diffraction (XRD) analysis**

Crystalline structures of all materials were identified by X-ray diffraction. Figure 1.1 shows XRD patterns of pure CeO₂, pure CuO and CeO₂-CuO nanocomposite. The

\[
d = \frac{0.9 \lambda}{\beta \cos \theta},
\]

where d is average crystallite size, λ is wavelength of Cu-Kα radiation (1.5406Å), β is full width at half maximum (FWHM) and θ is Bragg’s angle. It is seen from XRD that average crystallite size of CeO₂ was found to be 26 nm. The XRD spectrum exhibits an intense peak for (111) plane. The diffraction peaks of pure CuO at 2θ of 32.2°, 35.4°, 38.6°, 46.8°, 53.4°, 58.1°, 61.5°, 75.0° were respectively indexed as (111), (002), (112), (202), (113), (311), (023) planes which are in good agreement with CuO powder file (JCPDS no.80-1917) which corresponds to the monoclinic structure [28]. Further, no other impurity peak was observed in the XRD pattern, showing the single phase sample formation. It is seen from XRD that average crystallite size of CuO was found to be 25 nm. The lattice parameters calculated from the present data are a = 4.6890 Å, b = 3.425 Å and c = 5.1324 Å respectively, which are in good agreement with the reported data (JCPDS no.80-1917). From X-ray diffractogram of the CeO₂-CuO nanocomposite average crystallite size was found to be 10 nm. Decrease in crystallite size of composite as compare to pure nanoparticles shows formation of CeO₂-CuO nanocomposite.

**Scanning Electron Microscopy (SEM)**

Figure 2.1, 2.2 and 2.3 shows SEM micrographs of the CeO₂, CuO nanoparticles and CeO₂-CuO nanocomposite respectively, synthesized by microwave assisted sol-gel method. Homogeneous microstructures were observed for all the materials consisting of crystallites having various size and forms. The content has a great influence on the morphology and structure of the catalysts. The crystallite size estimated from SEM micrographs was found to be 30 µm for CeO₂ and CuO nanoparticles. While for CeO₂-CuO nanocomposite size comes out to be 10 µm. This variation in particle size strengthens with XRD analysis. It is clear from Fig. 2.1 that the CeO₂ formed is rich in the pores, which is composed of the CeO₂ crystallites [29]. It presents that particles are spherical in shape with a uniform size distribution. SEM image of CuO nanoparticles in Fig. 2.2 composed of small bulk particles. The CeO₂-CuO nanocomposite displays spongy-like features with large voids and small spherical agglomerates of CuO, as can be seen from SEM image shown in Fig. 2.3. These structures provide a large surface area and increase the electron transport. Such change in morphology creates voids and windows to generate wide porosity. The surface voids are formed due to the release of excessive volumes of gases upon the combustion reaction, introducing porosity to the prepared CeO₂-CuO nanocomposite materials, which results in reduction in the size of structural features [30]. Accordingly, we can observe the porosity of the samples increases from Fig. 2.1 to 2.3. However, such porous structure is useful in gas sensor application [31].

**Transmission Electron Microscopic (TEM) analysis**

TEM analysis gives information about size and morphology of CeO₂, CuO and CeO₂-CuO nanocomposite. The particle size of pure CeO₂ and pure CuO samples Fig.
The LPG Gas-Sensing Performance of CeO$_2$-CuO Nanocomposite Film Synthesized by Microwave Assisted Sol-Gel Method

3.1(a) and Fig. 3.2(a) are in the range of 20-30 nm, while for CeO$_2$-CuO nanocomposite Fig. 3.3(a) the particle size is 5-10 nm. TEM image of CeO$_2$ particles Fig. 3.1(a) show spherical morphology. The HRTEM image Fig. 3.1(b) shows lattice fringes which allows for identification of crystallographic spacing of CeO$_2$. It shows horizontal fringes. The fringe d = 0.32 nm matches with plane (111) of cubic CeO$_2$. The HRTEM image of CuO Fig. 3.2(b) shows lattice fringe d = 0.27 nm, which corresponds to (110) plane of monoclinic CuO. The TEM image of CeO$_2$-CuO nanocomposite Fig. 3.3(a) indicates that nanoparticles of CeO$_2$-CuO are well dispersed with smooth surface of uniform size and shows a homogenous particle distribution. Particles of two types are clearly shown in CeO$_2$-CuO nanocomposite. From HRTEM image Fig. 3.3(b), it implies that copper may be embedded in the lattice of ceria which can produce oxygen vacancies.

The selected area electron diffraction (SAED) pattern of CeO$_2$ nanoparticles, CuO nanoparticles and CeO$_2$-CuO nanocomposite showing in Fig. 3.1(c), 3.2(c), 3.3(c) respectively, discloses polymorphic distinct rings of the crystalline materials. High degree of crystallinity in polycrystals is confirmed from brightness of ring patterns of all samples. The SAED pattern confirms that nanoparticles are polycrystalline in nature. The SAED pattern in the Fig. 3.1(c) and Fig. 3.2(c) , also supports the d values obtained from XRD with rings which can be assigned to (111), (200), (220) and (311) planes of CeO$_2$ structure and (110), (002), (111) planes of CuO structure. The crystalline phases of TEM are in good agreement with XRD data.

UV-Visible technique was used to identify the absorption range and band gap energy of the composite material. The UV-Visible spectra of CeO$_2$, CuO nanoparticles and CeO$_2$-CuO nanocomposite is shown in Fig. 4.1. In pure samples absorption first increases in the ultraviolet region, then there is slow decrease in the ultraviolet region and then fast decreases in visible region. While in composite absorption first decreases, then slowly increases in ultraviolet region and then fast decreases in visible region. Pure CeO$_2$ gives three absorption peaks at 226 nm, 280 nm and 345 nm, respectively corresponding to O$^{2-}$→ Ce$^{3+}$ and O$^{2-}$→ Ce$^{4+}$ charge transfer transactions and inter bands appeared in CeO$_2$. Simultaneously, pure CuO shows a wide absorption peak at about 380 nm [29]. For CeO$_2$-CuO composite absorption bands appeared at 224 nm, 268 nm and 274 nm i.e. at lower wavelength as compared to pure oxides. From the absorption data, the band gap energy (E$_g$) of the material has been calculated using Tauc’s equation:

$$\alpha h\nu = A (h\nu - E_g)^n \quad \text{--- eq. (2)}$$

where $\alpha$ is the absorption coefficient and A is constant, h$\nu$ is the photon energy, E$_g$ is the optical band gap of the thin film. “n” is a number which characterizes the mechanism of a transition process, n = 1/2, 3/2 for direct transitions and 1, 2, 3 for indirect transitions. The Tauc’s plot was used for calculating the value of the direct optical energy band gap by extrapolating curve to zero absorption as shown in Fig. 4.2. The calculated value of band gap for CeO$_2$, CuO nanoparticles and CeO$_2$-CuO composite were found to be 3.19 eV, 1.7 eV and 1.3 eV respectively. The CeO$_2$-CuO composite shows very low band gap as compared to other materials. This reduction may be caused as results of additional sub-bandgap energy levels are induced with aid of abundant surface and interface defects.

References

Figure 4.1 UV-Visible Spectra of CeO$_2$, CuO Nanoparticles and CeO$_2$-CuO Nanocomposite.

Figure 4.2 Tauc’s plot for calculating the band gap energy of CeO$_2$, CuO Nanoparticles and CeO$_2$-CuO Nanocomposite.
within the nanoparticle formation [32]. Thus, the prepared film has a semiconducting nature.

![Figure 4.2 Tauc’s plot of the CeO2–CuO Nanocomposite showing the optical energy band gap.](Image)

**Gas sensing properties**

It is well known that CeO2 as well as CuO are two important kinds of fundamental materials and they have been broadly used as gas sensors. Furthermore, combining two materials will form heterojunction at the intergrain boundaries, which modifies the electronic transport. Hence, it is necessary to study the sensing properties of CeO2–CuO gas sensor. The gas sensing characteristics of the CeO2–CuO thin film have been investigated and the results are shown in here. Sensing parameters like sensitivity, percentage of sensor response, response and recovery time have been calculated from the sensing behaviour of the CeO2–CuO thin film. The gas sensor sensitivity was defined as the ratio of the current through the sample in air containing propane-butane mixture (LPG) at desired concentration to the current value in pure air atmosphere (I_{LPG} / I_{air}). In this case, at constant environmental conditions the value of the current through the sample changes significantly. The measurements were performed in the temperature range from 225°C to 325°C with 25°C step. The gas sensor tests have shown that an increase in propane-butane concentration leads to an increase in the current value. After the gas mixture introduction, the current dependencies have very similar character for all of the samples. It is necessary to point out, that the current value stabilizes after about 10 min. Figure 5.1 shows plot of sensitivity vs LPG concentration (in ppm) for different samples (CeO2, CuO and CeO2–CuO) at their operating temperature. Sensitivity is calculated by using following equation [33];

\[
\text{Sensitivity} = \frac{R_a}{R_g} \quad \text{eq. (3)}
\]

where \(R_a\) stands for the resistance of gas sensors in the reference gas (usually the air) and \(R_g\) stands for the resistance in the reference gas containing target gases. It is found that the sensitivity of the sensor increases as the concentration of LPG increases.

At 24 ppm of LPG concentration all samples show maximum sensitivity. After that, though the concentration of LPG increases sensitivity remains constant. The CeO2–CuO sensor shows maximum sensitivity as compared to pure samples. It is 2.08, 1.74, and 2.33 for CeO2, CuO and CeO2–CuO sensor respectively. Figure 5.2 shows plot of sensitivity as a function of operating temperature (in degree Celsius) for different samples (CeO2, CuO & CeO2 – CuO) for LPG at 24 ppm. The temperature of the sensor surface is one of the most influencing parameter. The optimum operating temperature for an effective sensor performance corresponds to that where the material is able to catalytically reduce or oxidize the target gas, simultaneously changing the electrical properties of the sensor material [34, 35]. In order to obtain the optimum operating temperature, the samples were exposed to 24 ppm LPG under different temperatures with the interval of 25°C. It is evident from figure that, percentage sensitivity increases at first and reaches its maximum value at the optimum temperature, then decrease with increase in temperature. Such behaviour can be explained by the kinetics and mechanics of gas reaction which occurred on the surface [36]. For low temperatures, the sensor response is confined by the speed of chemical reactions. For higher temperature, the sensor response is confined by the speed of the diffusion of gas molecules to that surface. Operating temperature for CeO2 and CuO is 300°C, while for CeO2–CuO it is 275°C. It reveals that, the CeO2–CuO sensor is more sensitive to LPG at lower operating temperature (275°C) than pure ones. If to order the samples according to their gas sensor sensitivity, we obtain: CuO/CeO2/CeO2–CuO. The result is quite sure from their morphology. The highest response has the sample CeO2–CuO that consists of small spherical agglomerates of CuO and has the largest value of the surface area to the volume ratio [26]. Gas Response (%) of CeO2, CuO and CeO2–CuO under different LPG concentration at its operating temperature is shown in Figure 5.3(a), 5.3(b) and 5.3(c) respectively. The resistance of the sensing film increased with respect to time on the exposure to LPG. Next, the sensing element reached a constant value (resistance) and then decreased due to the removal of LPG (recovery characteristics) from the gas chamber. Also, the sensing curves of the sensor are very broadening due to the increase of LPG concentration.
At low concentration, only few gas molecules would adsorb and it covers small area. However, on increasing the concentration, more number of gas molecules and oxygen species would adsorb at the surface of the sensing element, it covers large area of the material. Therefore, the sensitivity of the sensor was increased. It is shown that sensitivity of the CeO$_2$ based LPG sensors are linearly proportional to their specific surface area [36]. This process involves surface adsorption and reaction of reducing gases. The percentage of the sensor is given by following equation [33];

\[
\text{Percentage of sensor response} = \frac{R_s - R_f}{R_s} \times 100 \quad \text{--- eq. (4)}
\]

The sensitivity and percentage of the sensor response increased gradually with respect to the concentration of LPG. The maximum percentage of the sensor response was found to be 57.09% at 24 ppm of LPG for CeO$_2$-CuO, which is the highest response. For CeO$_2$ and CuO the percentage of the sensor response was 52.13% and 42.59% respectively. Moreover, the sensing curve has repeatability. Because ambient temperature and environmental conditions remain constant. Repeatability is defined as

**Table 1** Literature survey on LPG sensing performance of CeO$_2$-CuO Nanocomposite with reported materials

<table>
<thead>
<tr>
<th>Sr. No.</th>
<th>Material</th>
<th>Temperature °C</th>
<th>Sensitivity</th>
<th>Concentration ppm</th>
<th>References</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>SnO$_2$-CuO</td>
<td>264</td>
<td>0.79</td>
<td>500</td>
<td>37</td>
</tr>
<tr>
<td>2</td>
<td>Al-Ni-SnO$_2$</td>
<td>300</td>
<td>16</td>
<td>600</td>
<td>38</td>
</tr>
<tr>
<td>3</td>
<td>SnO$_2$</td>
<td>274</td>
<td>0.51</td>
<td>500</td>
<td>32</td>
</tr>
<tr>
<td>4</td>
<td>ZnO-CuO</td>
<td>500</td>
<td>0.9</td>
<td>400</td>
<td>39</td>
</tr>
<tr>
<td>5</td>
<td>CeO$_2$-CuO</td>
<td>275</td>
<td>2.33</td>
<td>24</td>
<td>Present work</td>
</tr>
</tbody>
</table>

The sensing element has ability to produce the same response for successive measurement and it is related to precision. Also, the repeatability reveals that the material permits an efficient and reliable LPG sensor. However, the LPG get fast adsorbed and diffused inside the sensing element. In the recovery sense, the gas desorbed gradually at room temperature and it took long time to recover. The sensing mechanism is based on the adsorption and desorption process at the surface of the sensing film [37, 38]. The environmental oxygen species adsorb on the surface of the CeO$_2$-CuO thin film. Then, takes out electron from the conduction band to form O$^-$ species that increases the resistance of the film. The reaction can be explained by the following equation,

\[
O_2^{\text{(gas)}} \leftrightarrow O_2^{\text{(ads)}} \quad \text{--- eq. (5)}
\]

\[
O_2^{\text{(ads)}} + e^- \rightarrow O_2^- \quad \text{--- eq. (6)}
\]

The chemisorbed oxygen reacts with LPG molecules. The above reaction would remove the adsorbed oxygen and then form gaseous species and water vapour. Also, the resistance of the film was changed. The following reaction has occurred between hydrocarbon and chemisorbed oxygen,

\[
2C_nH_{2n+2} + 2O_2^- \rightarrow 2C_nH_{2n}O + 2H_2O + 2e^- \quad \text{--- eq. (7)}
\]

where C$_n$H$_{2n+2}$ represents hydrocarbon. While LPG reacts with surface oxygen, the ignitable items exist, for example, water and potential barrier to charge transport must be created. The development of the potential barrier is expected to decrease the concentration of charge carriers (conduction). Thus increases the resistance of the film with time. In this way, the gas atoms were stopped and afterward oxygen in air would adsorb on the surface of the film (catch of electron). Thus decreases the resistance of the sensing film [32]. Table 1 shows a recent literature survey on LPG sensing performances of pure and composites. From this table, the prepared thin film sensor shows the high sensitivity and response. The results cited in Table 1 and the present work propose that nanocomposites are good candidates for gas sensors with high sensitivity and optimum temperature. Thus, the distinctive feature of our sample, in comparison to different LPG sensors reviewed in the literature is the absence of the characteristic maximum on the sensitivity versus temperature dependencies [39-42].

**Response and Recovery time**

The Response / Recovery time is an important parameter used for characterizing gas sensors. The time taken for the sensor to attain 90% of maximum change in resistance on exposure to the gas is the response time and the time taken by the sensor to get back 90% of original resistance is the recovery time. Figure 5.4 shows variations in LPG (24 ppm) response with time at temperature 275°C for CeO$_2$-CuO. The response was quick (~ 25 s) while the recovery time was (~ 50 s). The quick response may be due to faster oxidation of gas.

**CONCLUSION**

The experimental results showed that the CeO$_2$-CuO sensing film exhibited high sensitivity for the detection of LPG and the sensitivity depended on the composition of the composites, operating temperature etc. The larger surface area gives more response to react with the target gas. The film seems to be highly porous for oxygen adsorption. Also CuO isolates at the grain boundaries. The isolation of CuO around the boundary of CeO$_2$ forms a heterojunction between CeO$_2$ (n) and CuO (p), facilitating the efficient charge transfer, which enhances sensitivity [43]. The results revealed that, for LPG, the sensitivity of the CeO$_2$-CuO nanocomposites is better than CuO, ZnO, SnO$_2$, and Al-Ni-SnO$_2$.
CuO sensor is 2.33 at 275°C and it was higher than the pure ones. In addition, the dynamical gas sensor response at different temperature values and dependencies of the sensor sensitivity on the temperature at different LPG concentrations in air has been investigated. It has been found that sensor response depends on the sample morphology. If to order the samples according to their gas concentrations in air has been investigated. It has been found that sensor response depends on the sample.

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